

Catalysis Today 72 (2002) 251-257



# An examination of the role of plasma treatment for lean $NO_x$ reduction over sodium zeolite Y and gamma alumina Part 2. Formation of nitrogen

S. Yoon, A.G. Panov, R.G. Tonkyn, A.C. Ebeling, S.E. Barlow, M.L. Balmer\*

Pacific Northwest National Laboratory, Richland, WA, USA

#### **Abstract**

 $NO_x$  reduction with  $NO_2$  as the  $NO_x$  gas in the absence of plasma was compared to plasma treated lean  $NO_x$  exhaust where NO is converted to  $NO_2$  in the plasma. Product nitrogen was measured to prove true chemical reduction of  $NO_x$  to  $N_2$ . With plasma treatment, NO as the  $NO_x$  gas, and a NaY catalyst, the maximum conversion to nitrogen was 50% between 180 and 230 °C. The activity decreased at higher and lower temperatures. At 130 °C a complete nitrogen balance could be obtained, however between 164 and 227 °C less than 20% of the  $NO_x$  is converted to a nitrogen-containing compound or compounds not readily detected by gas chromatograph (GC) or Fourier transform infrared spectrometer (FT-IR) analysis. With plasma treatment,  $NO_2$  as the  $NO_x$  gas, and a NaY catalyst, a complete nitrogen balance is obtained with a maximum conversion to nitrogen of 55% at 225 °C.

For  $\gamma$ -alumina, with plasma treatment and NO<sub>2</sub> as the NO<sub>x</sub> gas, 59% of the NO<sub>x</sub> is converted to nitrogen at 340 °C. A complete nitrogen balance was obtained at these conditions. As high as 80% NO<sub>x</sub> removal over  $\gamma$ -alumina was measured by a chemiluminescent NO<sub>x</sub> meter with plasma treatment and NO as the NO<sub>x</sub> gas.

When NO is replaced with NO<sub>2</sub> and the simulated exhaust gases are not plasma treated, the maximum NO<sub>x</sub> reduction activity of NaY and  $\gamma$ -alumina decreases to 26 and 10%, respectively. This is a large reduction in activity compared to similar conditions where the simulated exhaust was plasma treated. Therefore, in addition to NO<sub>2</sub>, other plasma-generated species are required to maximize NO<sub>x</sub> reduction. © 2002 Elsevier Science B.V. All rights reserved.

Keywords: Plasma treatment; γ-Alumina; Chemiluminescent

# 1. Introduction

In recent years, plasma-assisted catalytic reduction of  $NO_x$  in lean and diesel exhaust was extensively studied [1–4]. In the previous paper [5] we discussed the effects of plasma processing on the composition of simulated diesel exhaust. The effect of tempera-

ture on the  $NO_x$  removal activity of NaY zeolite and  $\gamma$ -alumina was also examined.

It has been reported [1–5] that during plasma treatment of oxygen rich exhaust, NO is oxidized to NO<sub>2</sub>. Due to this oxidation step of the plasma, catalysts that utilize NO<sub>2</sub> are being investigated. Some groups have measured the activity of potential plasma-catalysts by simply replacing NO with NO<sub>2</sub> in the feed gas to simulate the plasma effect on the catalyst [6,7]. However, there are differences in activity and storage reported for similar catalysts when tested with NO<sub>2</sub> in simulated exhaust or with plasma treatment of simulated

<sup>\*</sup> Corresponding author. Present address. Caterpillar Inc., Technology Centre E/854, P.O. Box 1875, Peoria, IL 61656-1875, USA. Tel.: +1-309-587-4468; fax: +1-309-587-2953. E-mail address: balmer-millar\_lou@cat.com (M.L. Balmer).

exhaust. For example, Lampert showed that with an NO<sub>2</sub> feed and no plasma treatment a γ-alumina catalyst with 200 m<sup>2</sup>/g surface area converted less than 40% NO<sub>x</sub> to nitrogen at a space velocity of  $6000 \,\mathrm{h}^{-1}$ at 200 °C [6]. They measured up to 15% NO<sub>2</sub> storage and reported that the average conversion efficiency decreased to 20% at 14,400 h<sup>-1</sup>. Basic zeolites, Na-ZSM-5 and NaY were reported to primarily store  $NO_2$  with only 15%  $NO_x$  reduction activity at 200 °C. Conversely, Balmer et al. [8] and Yoon et al. [5] reported that at 200 °C activities as high as 70% can be achieved in plasma treated simulated exhaust streams followed by basic zeolites such as NaY with very little storage. Replacing NO with NO2 in the simulated lean  $NO_x$  exhaust, Penetrante et al. reports that the activity of  $\gamma$ -alumina can be greater than 90% at a temperature range of 300-550 °C [6]. Lastly, Vogtlin et al. [9] show 80% plasma-assisted catalytic reduction of  $NO_x$  with  $\gamma$ -Al<sub>2</sub>O<sub>3</sub> at 400 °C. The other effect of plasma is to oxidize hydrocarbons present in the exhaust. We found, that about 35% of propylene, used as a hydrocarbon source in the simulated diesel exhaust, is oxidized. Besides CO and CO<sub>2</sub> significant amount of aldehydes are formed [5]. The simultaneous decrease of the aldehydes and  $NO_x$  concentrations in the plasma-catalyst treated simulated exhaust suggests that the formation of aldehydes, as well as  $NO_2$ , is important for  $NO_x$ reduction performance of the plasma-catalyst systems.

The purpose of this study is to examine the significance of plasma, processing on  $NO_x$  reduction over  $\gamma$ -alumina and a basic zeolite, NaY.  $NO_x$  reduction with  $NO_2$  as the  $NO_x$  gas in the absence of plasma is compared to plasma treated lean  $NO_x$  exhaust where NO is converted to  $NO_2$  in the plasma. Therefore, the role of  $NO_2$ , the input hydrocarbon, and the hydrocarbon byproducts formed in the plasma are elucidated. True chemical  $NO_x$  reduction to  $N_2$  is measured for the zeolite and alumina catalyst by conducting nitrogen balance experiments in a helium carrier.

### 2. Experimental

### 2.1. Experimental plasma-catalyst apparatus

The experimental plasma-catalyst apparatus has been described earlier [5]. The system consists of a double dielectric-barrier discharge reactor followed by a quartz catalytic reactor tube. The catalytic reactor is capable of testing powders, pellets, and coated monoliths at various temperatures.

The plasma reactor temperature was maintained at  $110\,^{\circ}\text{C}$  for all tests to prevent water condensation. The catalyst reactor temperature was separately controlled. Extrudates of NaY (zeolyst) were tested;  $\gamma$ -alumina powder was pressed into pellets and sieved to 10–20 mesh.

Typical gas hourly space velocity (GHSV), calculated by dividing the standard gas flow rate by the catalyst bed volume, was  $12,000\,h^{-1}$  in the catalyst reactor. The typical GHSV within the plasma reactor was  $30,000-60,000\,h^{-1}$ . The effective operation of the plasma reactor is relatively insensitive to space velocity. The simulated exhaust used in this work was  $200\,\mathrm{ppm}$  of  $NO_x$ ,  $700\,\mathrm{ppm}$  of  $C_3H_6$ , 5% of  $O_2$  and 2% of  $H_2O$ . The balance gas was helium.

The effluent gas was analyzed by a chemiluminescent  $NO_x$  analyzer (CLNA) (Beckman Model 951), an MTI M200 micro gas chromatograph (GC), and a Fourier transform infrared spectrometer (FT-IR) (Nicolet Magna 560) equipped with a heated 2 m gas cell. For each FT-IR spectrum, 50 scans were collected at  $0.5 \, \mathrm{cm}^{-1}$  resolution. Measured absorbencies were converted to concentrations from calibration plots.

# 2.2. Nitrogen detection

With the typical simulated lean  $NO_x$  mix, true chemical reduction to N2 cannot be measured because the minor amount of N<sub>2</sub> produced from the  $NO_x$  reduction cannot be detected above the large nitrogen background. In order to detect N2 from the reduction reaction, experiments were conducted by replacing the nitrogen bath gas with helium. Previous work reported in Balmer et al. [10,11] has shown that while the energy efficiency is increased, the apparent gas phase chemistry is unchanged with helium. This result is expected since the background nitrogen does not play a role in the gas phase or surface chemistry. In addition, to simplify the GC measurements, CO and  $CO_2$  were removed from the simulated gas mix. Although these constituents will always be present in lean burn exhaust, Tonkyn et al. [12], has previously reported that neither CO nor CO<sub>2</sub> contribute significantly to the observed  $NO_x$  reduction chemistry. In

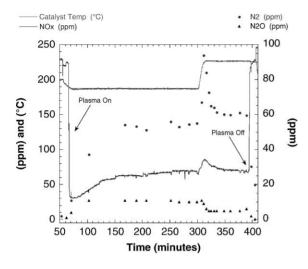


Fig. 1.  $NO_x$  concentration (ppm), catalyst temperature (°C),  $N_2$  concentration (ppm), and  $N_2O$  concentration (ppm) as a function of time with sodium zeolite Y and simplified lean  $NO_x$  exhaust. NO was used as the  $NO_x$  input at catalyst temperatures of 180 and 227 °C.

order to elucidate the role of the plasma products in  $NO_x$  reduction over the catalyst, nitrogen balance experiments were performed using both NO and  $NO_2$  as the  $NO_x$  input with and without plasma treatment of the gas.

# 2.2.1. NO as $NO_x$ input—Na zeolite Y (180–227°C)

First, sodium zeolite Y was examined with the simplified lean  $NO_x$  mix in helium at temperatures of 180–227 °C where the greatest  $NO_x$  conversion is observed [5]. NO was used as the input  $NO_x$  to confirm that the previously detected catalytic activity with NaY using a chemiluminescent  $NO_x$  meter was true chemical reduction to  $N_2$ . As shown in Fig. 1, when the simplified simulated exhaust was passed over the

NaY catalyst at a temperature of  $180^{\circ}$ C, no significant N<sub>2</sub> formation or NO<sub>x</sub> removal is observed until the plasma processing is initiated. An immediate drop in NO<sub>x</sub> concentration can be seen at 70 min when the plasma power was initiated and set at a power of 20 J/l.

The initial precipitous drop in  $NO_x$  concentration is followed by a slow rise in  $NO_x$  concentration until a steady-state value is reached at 250 min. Likewise, when the plasma is initiated, the  $N_2$  and  $N_2O$  production increases slowly with time until a steady-state value is reached at 250 min (Fig. 1). All of the  $NO_x$  leaving the catalyst is in the form of NO. Since the plasma reactor was operated at powers high enough to convert all of the input NO to  $NO_2$ , the catalyst converted a portion of the  $NO_2$  back to NO.

The measured concentrations of N2 and N2O out of the catalyst using GC analysis at their steady-state concentrations are shown in Table 1. The large time delay observed to reach a steady-state  $NO_x$  concentration is probably due to initial adsorption of NO<sub>x</sub>. Due to the large surface area of this catalyst, sufficient time is required until adsorption sites are completely saturated with NO<sub>x</sub>. Nitrogen and N<sub>2</sub>O production increase slowly over the time frame where  $NO_x$  adsorption is occurring, reaching steady-state at about the same time as the  $NO_x$  production. This result indicates that nitrogen production is correlated to the surface coverage of adsorbed  $NO_x$ . The steady-state  $N_2$  and  $N_2O$  (54+10 ppm) concentrations account for 81% of the missing nitrogen atoms at 180 °C. Therefore, 19% of the missing nitrogen atoms are neither N<sub>2</sub>, N<sub>2</sub>O, nor a  $NO_x$ .

Using a CLNA a steady-state  $NO_x$  reduction efficiency of 69% was measured. Therefore, replacing the  $N_2$  bath gas with helium did not affect the overall activity of NaY. Also, the activity was not negatively

Table 1 Summary of results from nitrogen balance experiments with sodium zeolite Y at various temperatures<sup>a</sup>

Catalyst temperature (°C)	NO <sub>x</sub> loss (%)	Nitrogen atoms missing (ppm)	[N <sub>2</sub> ] (ppm)	[N <sub>2</sub> O] (ppm)	Nitrogen recovered (%)	N <sub>2</sub> /N <sub>2</sub> O
NO as NO <sub>x</sub> input-	—Na zeolite Y					
130	44	107	39	15	100	3
164	55	132	41	8	74	5
180	69	158	54	10	81	5
227	69	158	59	5	81	12

<sup>&</sup>lt;sup>a</sup> Nitric oxide (NO) was used as the NO<sub>x</sub> input.

affected by the lack of CO<sub>2</sub> and CO in the simulated exhaust.

At 300 min, the catalyst temperature was increased from 180 to 227 °C. From Fig. 1, a small NO<sub>x</sub> desorption peak can be seen due to the temperature increase. Simultaneously, a burst of N2 is also observed. Some of the NO<sub>2</sub> initially stored on the NaY at the lower temperature desorbs as N2 as well as NO at the elevated temperature. At 227 °C the steady-state NO<sub>x</sub> efficiency is similar to the efficiency at 180 °C. The 54 ppm of N<sub>2</sub> detected at this temperature is 5 ppm higher than the N<sub>2</sub> concentration detected at 180 °C (Table 1). At the same time the  $N_2O$  detected at 227  $^{\circ}C$ is 5 ppm lower than the N<sub>2</sub>O concentration detected at 180 °C (Table 1). At higher temperatures, the reduction chemistry favors the formation of  $N_2$  over  $N_2O$ . The ratio of N2:N2O increases from 5 to 12 when the temperature is rised from 180 to 227 °C (Table 1). The overall nitrogen atoms accounted for are approximately 81% at both catalyst temperatures. Therefore, the formation of an undetected nitrogen-containing compound occurs at both temperatures. Possible products that could account for the undetected nitrogen include nitric acid (HNO<sub>3</sub>), hydrogen cyanide (HCN), or organo-nitrates such as methyl nitrate (CH<sub>3</sub>NO<sub>3</sub>). The detection and quantification of these species was beyond the scope of this study.

# 2.2.2. NO as $NO_x$ input gas—Na zeolite Y (130–164°C)

The nitrogen detection experiment with NaY was repeated at lower catalyst temperatures. A plot of the catalyst temperature,  $NO_x$  concentration,  $N_2$  and  $N_2O$ concentrations versus time are shown in Fig. 2. The behavior of the  $NO_x$  concentration is similar to that at higher temperatures. No initial conversion occurs at 130 °C without plasma treatment. When plasma processing is initiated, a dramatic drop in the measured NO<sub>x</sub> concentration is observed. The CLNA determined a steady-state conversion value of 44% at 130 °C (Table 1). The total nitrogen atoms missing as  $NO_x$  by the CLNA (107 ppm) and the total nitrogen atoms detected in the form of N2 and N2O (39 + 15 ppm) are approximately equivalent after 1 h at this temperature. Therefore 100% nitrogen balance is obtained.

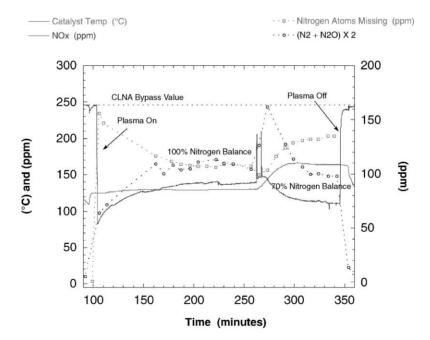


Fig. 2.  $NO_x$  concentration (ppm), catalyst temperature (°C), total nitrogen atoms missing (ppm), and total nitrogen atoms recovered in the form of  $N_2$  and  $N_2O$  (ppm) as a function of time with sodium zeolite Y and simplified lean  $NO_x$  exhaust. NO was used as the  $NO_x$  input at catalyst temperatures 130 and 164 °C.

Upon heating the catalyst to 164 °C a burst of NO<sub>x</sub> desorbtion was observed. After few minutes NO<sub>x</sub> concentration slowly declined to a lower steady-state value. Simultaneously, a burst of N2 was detected upon heating. At 164 °C, the steady-state NO<sub>x</sub> reduction efficiency by CLNA was determined to be 55%. The corresponding nitrogen atoms not detected as NO or NO<sub>2</sub> increased from 107 ppm at 130 °C to 132 ppm at 164 °C (Table 1). However, the amount of product nitrogen atoms detected as N2 and N2O slightly decreased, mainly due to a decrease in N2O concentration. Therefore, there is an incomplete nitrogen balance at 164 °C. It is interesting to note that the decrease in product nitrogen atoms is strictly due to less N<sub>2</sub>O formation at the higher temperature. The N<sub>2</sub> concentration increased slightly from 39 ppm at 130 °C to 41 ppm at the higher temperature, while the N<sub>2</sub>O concentration decreased from 15 to 8 ppm, respectively. This would suggest that there are competing pathways that lead to either N<sub>2</sub>O formation or to the formation of some other nitrogen-containing compound or compounds. From Table 1, it can be seen that the N2:N2O formation ratio decreases with increasing temperature.

# 2.2.3. $NO_2$ as $NO_x$ input—Na zeolite Y

The nitrogen detection experiment was repeated replacing NO with NO<sub>2</sub> as the NO<sub>x</sub> input gas and measuring N<sub>2</sub> formation with and without plasma treatment of the gas. The  $NO_x$  concentration by CLNA as well as the N<sub>2</sub> and N<sub>2</sub>O concentration by GC analysis as a function of time at 225 °C is shown in Fig. 3. Initially, the simulated lean burn exhaust bypassed the preheated catalyst bed. The catalyst was then exposed to the gas mix at 90 min. At this time, the majority of the NO2 was adsorbed on NaY. However, over the next hour increasing quantities of NO2 exited the catalyst bed until steady-state was reached (150 min). At steady-state, a large portion of the NO<sub>x</sub> leaving the catalyst is in the form of NO<sub>2</sub> (Fig. 3). The NO concentration increased slowly after the NO<sub>2</sub> was introduced to the catalyst. Even after the apparent steady-state  $NO_x$  concentration was reached, the NO concentration continued to rise. The N<sub>2</sub> and N<sub>2</sub>O concentrations followed the same trend as the NO<sub>x</sub> concentration increasing slowly up to 150 min. The chemiluminescent NO<sub>x</sub> meter measured a steady-state NO<sub>x</sub> efficiency of 26% or 46 ppm at 225 °C with NO<sub>2</sub>

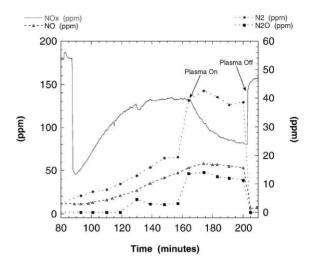


Fig. 3.  $NO_x$  concentration (ppm), NO concentration (ppm),  $N_2$  concentration (ppm), and  $N_2O$  concentration (ppm) as a function of time with sodium zeolite Y and simplified lean  $NO_x$  exhaust. NO was replaced with  $NO_2$  as the  $NO_x$  input. The catalyst temperature was set at  $225\,^{\circ}C$ .

as the  $NO_x$  feed gas and no plasma. Addition of  $N_2$  and  $N_2O$  concentrations results in 44 ppm of nitrogen atoms or essentially a complete nitrogen balance. A summary of the results and  $N_2$  and  $N_2O$  steady-state concentrations are shown in Table 2. The long rise time for  $N_2$  and  $N_2O$  concentrations and concurrent  $NO_x$  concentration indicates adequate time is required to achieve sufficient surface coverage to allow for reactions on the active sites of the catalyst.

Plasma processing was initiated at 160 min (Fig. 3). An immediate jump in the concentrations of  $N_2$  and  $N_2O$  were detected. The  $N_2$  concentration increased from 19 to 39 ppm and the  $N_2O$  concentration increased from 3 to 11 ppm, respectively (Table 2). In addition, the NO concentration began to level off and the total  $NO_x$  concentration slowly declined. After 40 min of plasma processing, the  $NO_x$  concentration continued to slowly decrease. At this point, with plasma and the NaY catalyst, the  $NO_x$  efficiency had increased to 55%. At 200 min, the  $N_2$  concentration was 39 ppm and the  $N_2O$  concentration was 11 ppm. At 55%  $NO_x$  efficiency, 100 ppm nitrogen atoms are missing, so a complete nitrogen balance was achieved with  $NO_2$  as the  $NO_x$  input combined with plasma processing.

This result shows that NO<sub>2</sub> is required in the reduction mechanism, however, propylene alone is not

342

Catalyst temperature (°C)	$NO_x$ loss (%)	Nitrogen atoms missing (ppm)	[N <sub>2</sub> ] (ppm)	[N <sub>2</sub> O] (ppm)	Nitrogen recovered (%)	$N_2/N_2O$
NO <sub>2</sub> as NO <sub>x</sub> input—Na zeo	olite Y (no plasma)					
225	26	46	19	3	96	6
NO <sub>2</sub> as NO <sub>x</sub> input—Na zeo	lite Y (with plasma)					
225	55	99	39	11	100	4
$NO_2$ as $NO_x$ input— $\gamma$ -alum	ina (no plasma)					
342	10	21				

66

128

Table 2 Summary of results from nitrogen balance experiments with sodium zeolite Y and  $\gamma$ -alumina with nitrogen dioxide (NO<sub>2</sub>) as the NO<sub>2</sub> input

an effective reductant in the reaction. It appears that partially-oxidized hydrocarbons created in the plasma play an essential role in the optimum performance of the catalyst.

# 2.3. $NO_2$ as $NO_x$ input— $\gamma$ -alumina

 $NO_2$  as  $NO_x$  input— $\gamma$ -alumina (with plasma)

The nitrogen detection experiment was also performed with the γ-alumina catalyst and NO<sub>2</sub> as the  $NO_x$  input. The results are summarized in Table 2. Without plasma, only 10% thermal activity was observed at a catalyst temperature of 342 °C. A large portion of the NO<sub>x</sub> exiting the catalyst was reduced to NO without the presence of plasma processing. When the plasma processing was initiated, the N<sub>2</sub> production immediately increased from 20 to 65 ppm. The N<sub>2</sub>O production remained low with plasma, similar to the N<sub>2</sub>O concentration with thermal activation. The  $NO_x$  concentration dropped immediately from 196 to 92 ppm with plasma and a steady-state value was achieved rather rapidly. The chemiluminescent NO<sub>x</sub> meter measurements revealed a steady-state NO<sub>x</sub> efficiency of 59% at 342 °C with plasma treatment compared to 10% with thermal activation alone (Table 2). At approximately 60% NO<sub>x</sub> efficiency, 128 ppm of nitrogen atoms are missing. With plasma processing, 66 ppm of N<sub>2</sub> and 2 ppm of N<sub>2</sub>O are detected resulting in a complete nitrogen balance.

The total  $NO_x$  concentration leaving the  $\gamma$ -alumina without plasma was 196 ppm and the  $NO:NO_2$  ratio is 1.8:1. So nearly two-thirds of the total  $NO_x$  has been reduced to NO and only 10% was reduced to nitrogen. When the plasma treatment was initiated, the total

 $NO_x$  concentration decreased to 89 ppm and the calculated  $NO:NO_2$  ratio leaving the catalyst decreased to 0.9:1. Without plasma, the majority of the  $NO_2$  is being reduced to NO and a small portion to nitrogen. With plasma processing, and in the presence of other plasma-generated species, a significant portion of the lost  $NO_2$  is reduced to  $N_2$ .

106

33

2

In summary, both  $\gamma$ -alumina and NaY catalysts have shown some NO $_x$  reduction with NO $_2$  as the NO $_x$  input gas. However, the activity is significantly enhanced with the addition of plasma processing. The data imply that species other than NO $_2$  formed in the plasma are also essential for optimum catalyst performance. It is likely that the important species are plasma-generated partially-oxidized hydrocarbons.

# 3. Conclusions

Plasma-assisted heterogeneous catalysis has been shown to be an effective process in the remediation of  $NO_x$  in synthetic lean burn gasoline and diesel compression ignition exhaust. This study was undertaken to examine the role of plasma processing on lean  $NO_x$  reduction over NaY and  $\gamma$ -alumina.

Product nitrogen was measured to prove true chemical reduction of  $NO_x$  to  $N_2$ . For  $N_2$  detection experiments, the  $N_2$  bath gas of a simplified simulated lean  $NO_x$  exhaust was replaced with He to allow for detection of  $N_2$  and  $N_2O$  formation after the catalyst. It was shown that true chemical reduction to nitrogen is the dominant reaction over NaY. At 130 °C a complete nitrogen balance can be obtained, however between 164

and 227 °C less than 20% of the reduced  $NO_x$  formed on NaY produces a nitrogen-containing compound or compounds not detected by GC or FT-IR analysis.

Nitrogen detection experiments were also conducted replacing the typical NO for the  $NO_x$  input with  $NO_2$ . This was done to examine the role of  $NO_2$  with and without plasma processing. It was shown that  $NO_2$  is slightly active with propylene as the reductant with NaY and  $\gamma$ -alumina. However, the activity is greatly enhanced with plasma processing, suggesting that in addition to  $NO_2$ , other plasma-generated species are important for  $NO_x$  reduction. A complete nitrogen balance was obtained for both NaY and  $\gamma$ -alumina with a  $NO_2$  feed.

#### References

- J. Hoard, H. Servati (Eds.), Plasma Exhaust After Treatment, SAE SP-1395, Society of Automotive Engineers, 1998.
- [2] M. Lou Balmer, G. Fisher, J. Hoard (Eds.), Non-Thermal Plasma Exhaust Emission Control, SAE SP-1483, Society of Automotive Engineers, 1999.
- [3] M. Lou Balmer, G. Fisher, J. Hoard (Eds.), Non-Thermal Plasma, SAE SP-1395, Society of Automotive Engineers, 1999
- [4] B.M. Penetrante, S.E. Schultheis (Eds.), Non-Thermal Plasma Techniques for Pollution Control—Part A: Overview,

- Fundamentals and Supporting Technologies, Springer, Berlin, 1993
- [5] S. Yoon, R.G. Tonkyn, A.G. Panov, A.C. Ebeling, S.E. Barlow, M.L. Balmer, Topics in Catalysis, submitted for publication.
- [6] B.M. Penetrante, R.M. Brusasco, B.T. Merritt, W.J. Pitz, G.E. Vogtlin, M.C. Kung, H.H. Kung, C.Z. Wan, K.E. Voss, Plasma-Assisted Catalytic Reduction of NO<sub>x</sub>, SAE 982508, 1998
- [7] Jordan K. Lampert, An Assessment of the Plasma Assisted Catalytic Reactor (PACR) Approach to Lean NO<sub>x</sub> Abatement: The Relative Reducibility of NO and NO<sub>2</sub> using #2 Diesel Fuel as the Reductant, SAE 2000-01-2962, 2000.
- [8] M.L. Balmer, R.G. Tonkyn, A.Y. Kim, I.S. Yoon, D. Jimenez, T. Orlando, S.E. Barlow, J. Hoard, Diesel NO<sub>x</sub> Reduction on Surfaces in Plasma, SAE 982511, 1998.
- [9] G.E. Vogtlin, B.T. Merritt, M.C. Hsiao, P.H. Wallman, B.M. Penetrante, Plasma-Assisted Catalytic Reduction System, U.S. Patent 5,711,147 (1998).
- [10] M.L. Balmer, R.G. Tonkyn, A.Y. Kim, J. Hoard, I.S. Yoon, D. Jimenez, T. Orlando, S.E. Barlow, Nitrogen measurement from NO<sub>x</sub> reduction for a plasma-catalyst system in simulated diesel exhaust, in: Proceedings of the 1998 Diesel Engine Emissions Reduction Workshop in Castine, Maine, July 1998.
- [11] M.L. Balmer, R.G. Tonkyn, I.S. Yoon, A. Kolwaite, S.E. Barlow, G. Maupin, J. Hoard NO<sub>x</sub> Destruction Behavior of Select Materials When Combined with a Non-Thermal Plasma, SAE 1999-01-3640, October 1999.
- [12] R.G. Tonkyn, S.E. Barlow, M.L. Balmer, T. Orlando, J. Hoard, D. Goulette, Vehicle Exhaust Treatment Using Electrical Dishcharge Methods, SAE 971716, May 1997.